

# **SWITCHMODE™ II Series NPN Silicon Power Transistors**

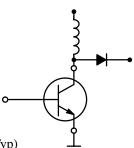
The BUV48/BUV48A transistors are designed for high-voltage, high-speed, power switching in inductive circuits where fall time is critical. They are particularly suited for line-operated SWITCHMODE applications such as:

- Switching Regulators
- Inverters
- Solenoid and Relay Drivers
- Motor Controls
- Deflection Circuits
- Fast Turn-Off Times

60 ns Inductive Fall Time — 25°C (Typ) 120 ns Inductive Crossover Time — 25°C (Typ)

- Operating Temperature Range –65 to +175°C
- 100°C Performance Specified for:

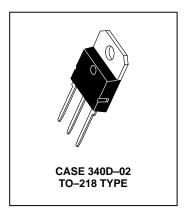
Reverse–Biased SOA with Inductive Loads Switching Times with Inductive Loads Saturation Voltage Leakage Currents (125°C)



# BUV48 BUV48A

15 AMPERES
NPN SILICON
POWER TRANSISTORS
400 AND 450 VOLTS  $V_{(BR)CEO}$ 850-1000 VOLTS  $V_{(BR)CEX}$ 

150 WATTS



#### **MAXIMUM RATINGS**

Rating	Symbol	BUV48	BUV48A	Unit
Collector–Emitter Voltage	V <sub>CEO(sus)</sub>	400	450	Vdc
Collector–Emitter Voltage (V <sub>BE</sub> = -1.5 V)	V <sub>CEX</sub>	850	1000	Vdc
Emitter Base Voltage	V <sub>EB</sub>	7		Vdc
Collector Current — Continuous — Peak (1) — Overload	Ic I <sub>CM</sub> I <sub>OI</sub>	15 30 60		Adc
Base Current — Continuous — Peak (1)	I <sub>B</sub>	5 20		Adc
Total Power Dissipation — T <sub>C</sub> = 25°C — T <sub>C</sub> = 100°C Derate above 25°C	P <sub>D</sub>	150 75 1		Watts W/°C
Operating and Storage Junction Temperature Range	T <sub>J</sub> , T <sub>stg</sub>	−65 to	+175	°C

#### THERMAL CHARACTERISTICS

Characteristic	Symbol	Max	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	1	°C/W
Maximum Lead Temperature for Soldering Purposes: 1/8" from Case for 5 Seconds	TL	275	°C

<sup>(1)</sup> Pulse Test: Pulse Width = 5 ms, Duty Cycle ≤ 10%.

# **ELECTRICAL CHARACTERISTICS** (T<sub>C</sub> = 25°C unless otherwise noted)

Characteristic	Symbol	Min	Тур	Max	Unit	
OFF CHARACTERISTICS (1)						
Collector–Emitter Sustaining Voltage (Table 1) $(I_C = 200 \text{ mA}, I_B = 0) \text{ L} = 25 \text{ mH}$	BUV48 BUV48A	V <sub>CEO(sus)</sub>	400 450		_	Vdc
Collector Cutoff Current $(V_{CEX} = Rated \ Value, \ V_{BE(off)} = 1.5 \ Vdc)$ $(V_{CEX} = Rated \ Value, \ V_{BE(off)} = 1.5 \ Vdc, \ T_C = 125 ^{\circ}C)$		I <sub>CEX</sub>	_		0.2 2	mAdc
Collector Cutoff Current ( $V_{CE}$ = Rated $V_{CEX}$ , $R_{BE}$ = 10 $\Omega$ )	T <sub>C</sub> = 25°C T <sub>C</sub> = 125°C	I <sub>CER</sub>		_	0.5 3	mAdc
Emitter Cutoff Current $(V_{EB} = 5 \text{ Vdc}, I_C = 0)$		I <sub>EBO</sub>	_	_	0.1	mAdc
Emitter–Base Breakdown Voltage (I <sub>E</sub> = 50 mA – I <sub>C</sub> = 0)		V <sub>(BR)EBO</sub>	7	_	_	Vdc
SECOND BREAKDOWN		<b>.</b>		•		1
Second Breakdown Collector Current with Base Forward	Biased	I <sub>S/b</sub>	S	See Figure 1	2	
Clamped Inductive SOA with Base Reverse Biased		RBSOA	S	See Figure 1	3	
ON CHARACTERISTICS (1)		1	I			1
DC Current Gain		h <sub>FE</sub>				
$(I_C = 10 \text{ Adc}, V_{CE} = 5 \text{ Vdc})$ $(I_C = 8 \text{ Adc}, V_{CE} = 5 \text{ Vdc})$	BUV48 BUV48A		8 8	_		
Collector–Emitter Saturation Voltage $ \begin{aligned} &(I_C=10 \text{ Adc, } I_B=2 \text{ Adc}) \\ &(I_C=15 \text{ Adc, } I_B=3 \text{ Adc}) \\ &(I_C=15 \text{ Adc, } I_B=3 \text{ Adc}) \\ &(I_C=10 \text{ Adc, } I_B=2 \text{ Adc, } T_C=100^{\circ}\text{C}) \\ &(I_C=8 \text{ Adc, } I_B=1.6 \text{ Adc}) \\ &(I_C=12 \text{ Adc, } I_B=2.4 \text{ Adc}) \\ &(I_C=8 \text{ Adc, } I_B=1.6 \text{ Adc, } T_C=100^{\circ}\text{C}) \end{aligned} $	BUV48 BUV48A	VCE(sat)		_ _ _ _ _	1.5 5 2 1.5 5	Vdc
Base–Emitter Saturation Voltage ( $I_C$ = 10 Adc, $I_B$ = 2 Adc) ( $I_C$ = 10 Adc, $I_B$ = 2 Adc, $T_C$ = 100°C) ( $I_C$ = 8 Adc, $I_B$ = 1.6 Adc) ( $I_C$ = 8 Adc, $I_B$ = 1.6 Adc, $T_C$ = 100°C)	BUV48 BUV48A	V <sub>BE(sat)</sub>	_ _ _ _	_ _ _ _	1.6 1.6 1.6 1.6	Vdc
DYNAMIC CHARACTERISTICS		_		-		-
Output Capacitance $(V_{CB} = 10 \text{ Vdc}, I_E = 0, f_{test} = 1 \text{ MHz})$		C <sub>ob</sub>	_	_	350	pF
SWITCHING CHARACTERISTICS Resistive Load (Table 1)						
Delay Time		t <sub>d</sub>	_	0.1	0.2	μs
Rise Time I <sub>C</sub> = 10 A, I <sub>B</sub> , = 2 A I <sub>C</sub> = 8 A, I <sub>B</sub> , = 1.6 A	BUV48 BUV48A	t <sub>r</sub>	_	0.4	0.7	
Storage Time Duty Cycle ≤ 2%, V <sub>BE(off)</sub> = 5 V	2011011	t <sub>s</sub>	_	1.3	2	
Fall Time $T_p = 30 \mu s$ , $V_{CC} = 300 \text{ V}$		t <sub>f</sub>	_	0.2	0.4	1
			I	1	I	1
Inductive Load, Clamped (Table 1)			1			
Inductive Load, Clamped (Table 1) Storage Time		t <sub>sv</sub>	_	1.3	_	μs
Storage Time I <sub>C</sub> = 10 A BUV48	(T <sub>C</sub> = 25°C)			0.06	_	μς
Storage Time	(T <sub>C</sub> = 25°C)	t <sub>fi</sub>	_ _ _			μs
Storage Time $I_C = 10 \text{ A}$ BUV48 $I_{B1} = 2 \text{ A}$	$(T_C = 25^{\circ}C)$ $(T_C = 100^{\circ}C)$			0.06		μs - -

<sup>(1)</sup> Pulse Test: Pulse Width = 300  $\mu$ s, Duty Cycle  $\leq$  2%. Vcl = 300 V, V<sub>BE(off)</sub> = 5 V, Lc = 180  $\mu$ H

# **DC CHARACTERISTICS**

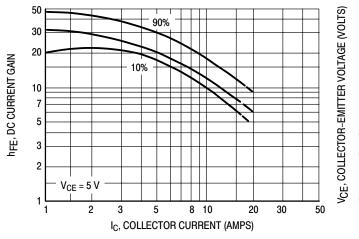
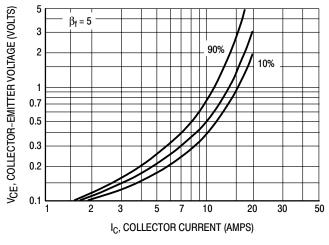


Figure 1. DC Current Gain

Figure 2. Collector Saturation Region



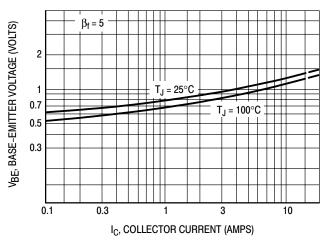
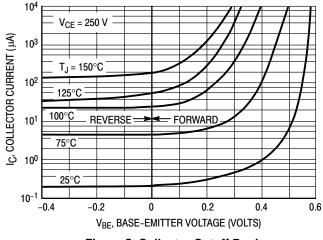


Figure 3. Collector-Emitter Saturation Voltage

Figure 4. Base-Emitter Voltage



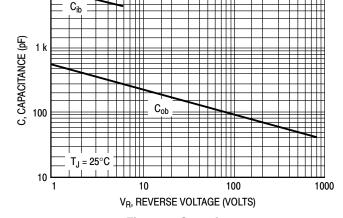
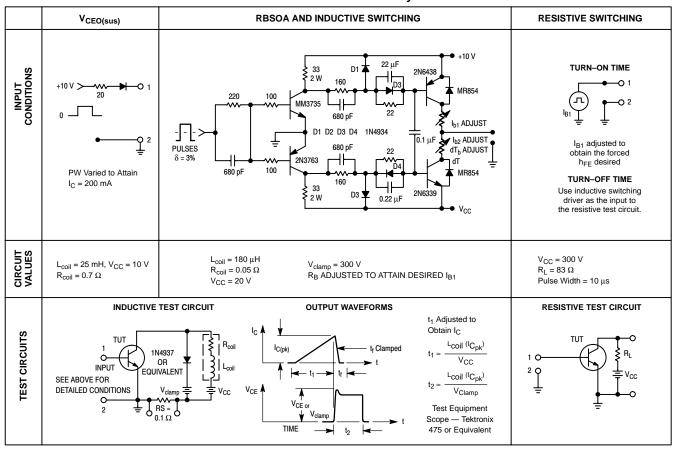


Figure 5. Collector Cutoff Region

Figure 6. Capacitance

10 k

**Table 1. Test Conditions for Dynamic Performance** 



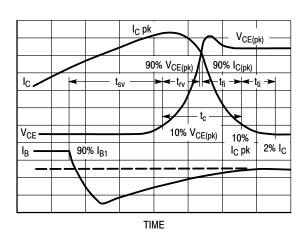


Figure 7. Inductive Switching Measurements

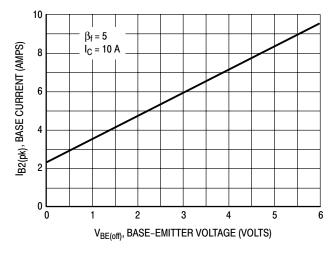


Figure 8. Peak-Reverse Current

#### **SWITCHING TIMES NOTE**

In resistive switching circuits, rise, fall, and storage times have been defined and apply to both current and voltage waveforms since they are in phase. However, for inductive loads which are common to SWITCHMODE power supplies and hammer drivers, current and voltage waveforms are not in phase. Therefore, separate measurements must be made on each waveform to determine the total switching time. For this reason, the following new terms have been defined.

t<sub>sv</sub> = Voltage Storage Time, 90% I<sub>B1</sub> to 10% V<sub>clamp</sub>

 $t_{rv}$  = Voltage Rise Time, 10–90%  $V_{clamp}$ 

 $t_{fi}$  = Current Fall Time, 90–10%  $I_C$ 

 $t_{ti}$  = Current Tail, 10–2%  $I_C$ 

 $t_c$  = Crossover Time, 10%  $V_{clamp}$  to 10%  $I_C$ 

An enlarged portion of the inductive switching waveforms is shown in Figure 7 to aid in the visual identity of these terms.

For the designer, there is minimal switching loss during storage time and the predominant switching power losses occur during the crossover interval and can be obtained using the standard equation from AN–222:

$$P_{SWT} = 1/2 V_{CC}I_{C}(t_{c}) f$$

In general,  $t_{rv} + t_{fi} \approx t_c$ . However, at lower test currents this relationship may not be valid.

As is common with most switching transistors, resistive switching is specified at 25°C and has become a benchmark for designers. However, for designers of high frequency converter circuits, the user oriented specifications which make this a "SWITCHMODE" transistor are the inductive switching speeds (t<sub>c</sub> and t<sub>sv</sub>) which are guaranteed at 100°C.

#### **INDUCTIVE SWITCHING**

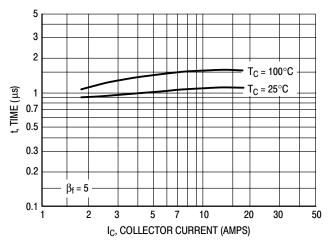


Figure 9. Storage Time, tsv

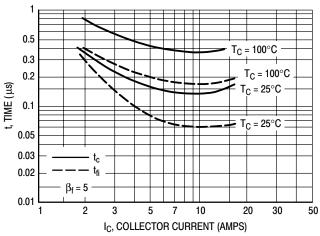


Figure 10. Crossover and Fall Times

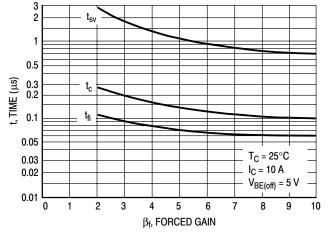


Figure 11. Turn-Off Times versus Forced Gain

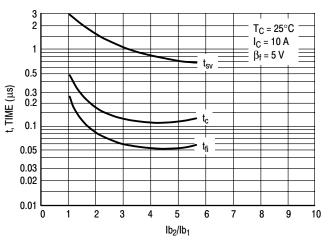


Figure 12. Turn-Off Times versus Ib<sub>2</sub>/Ib<sub>1</sub>

The Safe Operating Area figures shown in Figures 12 and 13 are specified for these devices under the test conditions shown.

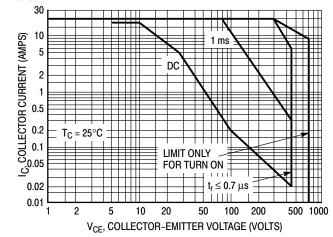


Figure 13. Forward Bias Safe Operating Area

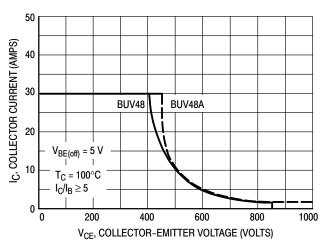


Figure 14. Reverse Bias Safe Operating Area

#### SAFE OPERATING AREA INFORMATION

#### **FORWARD BIAS**

There are two limitations on the power handling ability of a transistor: average junction temperature and second breakdown. Safe operating area curves indicate  $I_C - V_{CE}$  limits of the transistor that must be observed for reliable operation; i.e., the transistor must not be subjected to greater dissipation than the curves indicate.

The data of Figure 13 is based on  $T_C = 25^{\circ}C$ ;  $T_{J(pk)}$  is variable depending on power level. Second breakdown pulse limits are valid for duty cycles to 10% but must be derated when  $T_C \leq 25^{\circ}C$ . Second breakdown limitations do not derate the same as thermal limitations. Allowable current at the voltages shown on Figure 13 may be found at any case temperature by using the appropriate curve on Figure 15.

 $T_{J(pk)}$  may be calculated from the data in Figure 11. At high case temperatures, thermal limitations will reduce the power that can be handled to values less than the limitations imposed by second breakdown.

#### **REVERSE BIAS**

For inductive loads, high voltage and high current must be sustained simultaneously during turn-off, in most cases, with the base to emitter junction reverse biased. Under these conditions the collector voltage must be held to a safe level at or below a specific value of collector current. This can be accomplished by several means such as active clamping, RC snubbing, load line shaping, etc. The safe level for these devices is specified as Reverse Bias Safe Operating Area and represents the voltage current conditions during reverse biased turn-off. This rating is verified under clamped conditions so that the device is never subjected to an avalanche mode. Figure 14 gives RBSOA characteristics.

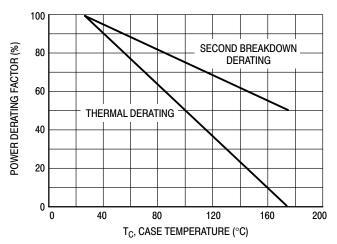


Figure 15. Power Derating

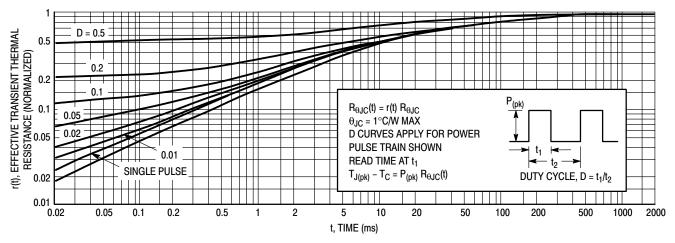


Figure 16. Thermal Response

# **OVERLOAD CHARACTERISTICS**

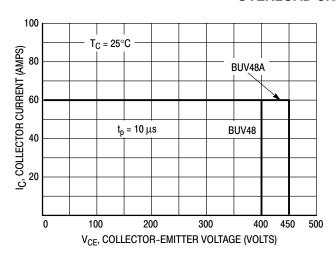


Figure 17. Rated Overload Safe Operating Area (OLSOA)

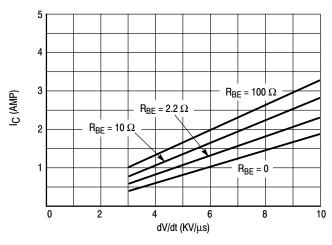


Figure 18.  $I_C = f(dV/dt)$ 

## OLSOA

OLSOA applies when maximum collector current is limited and known. A good example is a circuit where an inductor is inserted between the transistor and the bus, which limits the rate of rise of collector current to a known value. If the transistor is then turned off within a specified amount of time, the magnitude of collector current is also known.

Maximum allowable collector—emitter voltage versus collector current is plotted for several pulse widths. (Pulse width is defined as the time lag between the fault condition and the removal of base drive.) Storage time of the transistor has been factored into the curve. Therefore, with bus voltage and maximum collector current known, Figure 17 defines the maximum time which can be allowed for fault detection and shutdown of base drive.

OLSOA is measured in a common-base circuit (Figure 19) which allows precise definition of collector-emitter voltage and collector current. This is the same circuit that is used to measure forward-bias safe operating area.

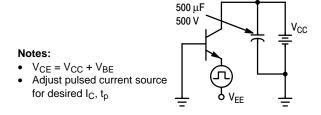
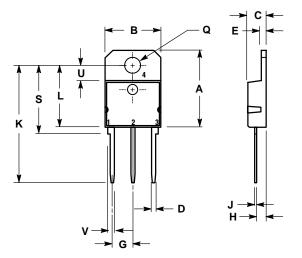


Figure 19. Overload SOA Test Circuit

#### PACKAGE DIMENSIONS

SOT-93 (TO-218) CASE 340D-02 ISSUE B



#### NOTES:

- DIMENSIONING AND TOLERANCING PER ANSI
   V14 5M 1982
- Y14.5M, 1982. 2. CONTROLLING DIMENSION: MILLIMETER.

	MILLIMETERS		INCHES		
DIM	MIN	MAX	MIN	MAX	
Α		20.35		0.801	
В	14.70	15.20	0.579	0.598	
С	4.70	4.90	0.185	0.193	
D	1.10	1.30	0.043	0.051	
Е	1.17	1.37	0.046	0.054	
G	5.40	5.55	0.213	0.219	
Н	2.00	3.00	0.079	0.118	
J	0.50	0.78	0.020	0.031	
K	31.00 REF		1.220 REF		
L		16.20		0.638	
Q	4.00	4.10	0.158	0.161	
S	17.80	18.20	0.701	0.717	
U	4.00 REF		0.157 REF		
٧	1.75 REF		0.069		

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