

FEATURES

- 100MHz Gain Bandwidth Product
- 750V/ μ s Slew Rate
- 3.6mA Maximum Supply Current per Amplifier
- Tiny 3mm x 3mm x 0.8mm DFN Package
- 8nV/ $\sqrt{\text{Hz}}$ Input Noise Voltage
- Unity-Gain Stable
- 1.5mV Maximum Input Offset Voltage
- 4 μ A Maximum Input Bias Current
- 400nA Maximum Input Offset Current
- 40mA Minimum Output Current, $V_{OUT} = \pm 3\text{V}$
- $\pm 3.5\text{V}$ Minimum Input CMR, $V_S = \pm 5\text{V}$
- 30ns Settling Time to 0.1%, 5V Step
- Specified at $\pm 5\text{V}$, Single 5V Supplies
- Operating Temperature Range: -40°C to 85°C

APPLICATIONS

- Active Filters
- Wideband Amplifiers
- Buffers
- Video Amplification
- Communication Receivers
- Cable Drivers
- Data Acquisition Systems

DESCRIPTION

The LT[®]1813/LT1814 are dual and quad, low power, high speed, very high slew rate operational amplifiers with excellent DC performance. The LT1813/LT1814 feature reduced supply current, lower input offset voltage, lower input bias current and higher DC gain than other devices with comparable bandwidth. The circuit topology is a voltage feedback amplifier with the slewing characteristics of a current feedback amplifier.

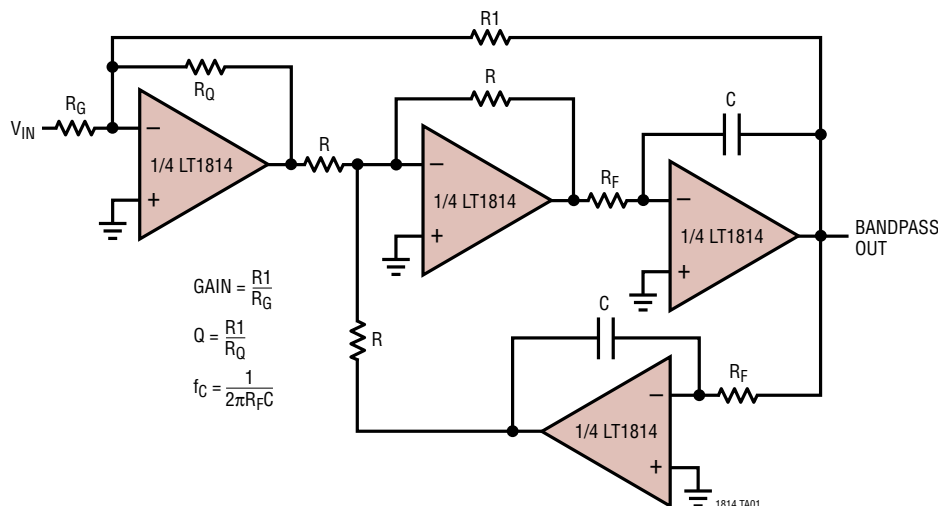
The output drives a 100 Ω load to $\pm 3.5\text{V}$ with $\pm 5\text{V}$ supplies. On a single 5V supply, the output swings from 1.1V to 3.9V with a 100 Ω load connected to 2.5V. The amplifiers are stable with a 1000pF capacitive load making them useful in buffer and cable driver applications.

The LT1813/LT1814 are manufactured on Linear Technology's advanced low voltage complementary bipolar process. The LT1813 dual op amp is available in 8-pin MSOP, SO and 3mm x 3mm low profile (0.8mm) dual fine pitch leadless packages (DFN). The quad LT1814 is available in 14-pin SO and 16-pin SSOP packages. A single version, the LT1812, is also available (see separate data sheet).

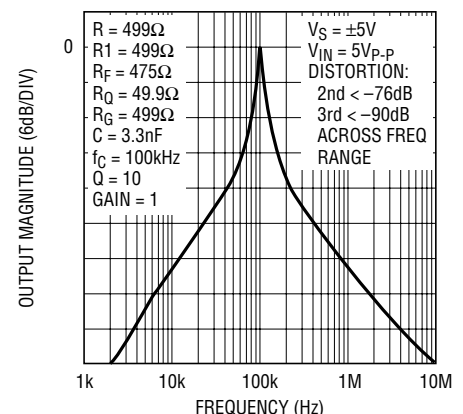
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TYPICAL APPLICATION

Bandpass Filter with Independently Settable Gain, Q and f_c



Filter Frequency Response



LT1813/LT1814

ABSOLUTE MAXIMUM RATINGS (Note 1)

Total Supply Voltage (V^+ to V^-)

LT1813/LT1814 12.6V

LT1813HV 13.5V

Differential Input Voltage (Transient Only, Note 2) .. $\pm V_S$

Input Voltage $\pm V_S$

Output Short-Circuit Duration (Note 3) Indefinite

Operating Temperature Range -40°C to 85°C

Specified Temperature Range (Note 8) .. -40°C to 85°C

Maximum Junction Temperature 150°C

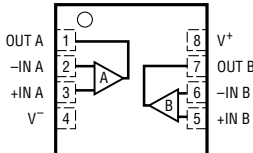
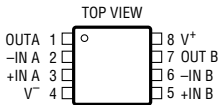
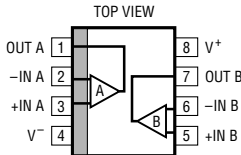
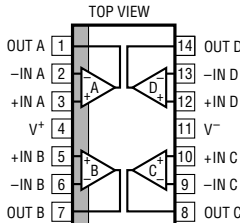
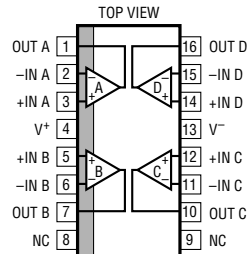
(DD Package) 125°C

Storage Temperature Range -65°C to 150°C

(DD Package) -65°C to 125°C

Lead Temperature (Soldering, 10 sec) 300°C

PACKAGE/ORDER INFORMATION

TOP VIEW  DD PACKAGE 8-LEAD (3mm x 3mm) PLASTIC DFN $T_{JMAX} = 125^{\circ}\text{C}$, $\theta_{JA} = 160^{\circ}\text{C/W}$ UNDERSIDE METAL INTERNALLY CONNECTED TO V^-		ORDER PART NUMBER LT1813DDD* LT1813CDD LT1813IDD DD PART MARKING ** LAAQ		TOP VIEW  MS8 PACKAGE 8-LEAD PLASTIC MSOP $T_{JMAX} = 150^{\circ}\text{C}$, $\theta_{JA} = 250^{\circ}\text{C/W}$ ORDER PART NUMBER LT1813DMS8* MS8 PART MARKING LTGZ	
TOP VIEW  S8 PACKAGE 8-LEAD PLASTIC SO $T_{JMAX} = 150^{\circ}\text{C}$, $\theta_{JA} = 150^{\circ}\text{C/W}$		TOP VIEW  S PACKAGE 14-LEAD PLASTIC SO $T_{JMAX} = 150^{\circ}\text{C}$, $\theta_{JA} = 110^{\circ}\text{C/W}$		TOP VIEW  GN PACKAGE 16-LEAD PLASTIC SSOP $T_{JMAX} = 150^{\circ}\text{C}$, $\theta_{JA} = 135^{\circ}\text{C/W}$	
ORDER PART NUMBER	S8 PART MARKING	ORDER PART NUMBER	ORDER PART NUMBER		
LT1813DS8*	1813D	LT1814CS	LT1814CGN		
LT1813CS8	1813	LT1814IS	LT1814IGN		
LT1813IS8	1813I		GN PART MARKING		
LT1813HVD8*	813HVD		1814		
LT1813HVCS8	1813HV		1814I		
LT1813HVIS8	813HVI				

Consult LTC marketing for parts specified with wider operating temperature ranges. *See Note 9.

**The temperature grades are identified by a label on the shipping container.

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V_S = \pm 5\text{V}$, $V_{CM} = 0\text{V}$, unless otherwise noted. (Note 8)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
V_{OS}	Input Offset Voltage (Note 4)	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	0.5	1.5	mV
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		2	mV
					3	mV
$\frac{\Delta V_{OS}}{\Delta T}$	Input Offset Voltage Drift (Note 7)	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	10	15	$\mu\text{V}/^\circ\text{C}$
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	10	30	$\mu\text{V}/^\circ\text{C}$
I_{OS}	Input Offset Current	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	50	400	nA
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		500	nA
					600	nA
I_B	Input Bias Current	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	-0.9	± 4	μA
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		± 5	μA
					± 6	μA
e_n	Input Noise Voltage Density	$f = 10\text{kHz}$		8		$\text{nV}/\sqrt{\text{Hz}}$
i_n	Input Noise Current Density	$f = 10\text{kHz}$		1		$\text{pA}/\sqrt{\text{Hz}}$
R_{IN}	Input Resistance	$V_{CM} = 3.5\text{V}$ Differential		3	10	$\text{M}\Omega$
					1.5	$\text{M}\Omega$
C_{IN}	Input Capacitance			2		pF
V_{CM}	Input Voltage Range	Guaranteed by CMRR $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	± 3.5	± 4.2	V
				± 3.5		V
CMRR	Common Mode Rejection Ratio	$V_{CM} = \pm 3.5\text{V}$		75	85	dB
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	73		dB
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	72		dB
PSRR	Power Supply Rejection Ratio	Guaranteed by PSRR $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	± 1.25	± 2	V
					± 2	V
A_{VOL}	Large-Signal Voltage Gain	$V_{OUT} = \pm 3\text{V}$, $R_L = 500\Omega$ $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	78	97	dB
			●	76		dB
			●	75		dB
		$V_{OUT} = \pm 3\text{V}$, $R_L = 100\Omega$ $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	75	97	dB
			●	73		dB
			●	72		dB
V_{OUT}	Maximum Output Swing (Positive/Negative)	$R_L = 500\Omega$, 30mV Overdrive $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	1.5	3	V/mV
			●	1.0		V/mV
			●	0.8		V/mV
		$R_L = 100\Omega$, 30mV Overdrive $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	1.0	2.5	V/mV
			●	0.7		V/mV
			●	0.6		V/mV
V_{OUT}	Maximum Output Swing (Positive/Negative)	$R_L = 500\Omega$, 30mV Overdrive $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	± 3.8	± 4	V
			●	± 3.7		V
			●	± 3.6		V
		$R_L = 100\Omega$, 30mV Overdrive $T_A = 0^\circ\text{C to } 70^\circ\text{C}$ $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	± 3.35	± 3.5	V
			●	± 3.25		V
			●	± 3.15		V

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V_S = \pm 5\text{V}$, $V_{CM} = 0\text{V}$, unless otherwise noted. (Note 8)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
I_{OUT}	Maximum Output Current	$V_{OUT} = \pm 3\text{V}$, 30mV Overdrive $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	± 40 ± 35 ± 30	± 60		mA mA mA
I_{SC}	Output Short-Circuit Current	$V_{OUT} = 0\text{V}$, 1V Overdrive (Note 3) $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	± 75 ± 60 ± 55	± 100		mA mA mA
SR	Slew Rate	$A_V = -1$ (Note 5) $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	500 400 350	750		V/ μs V/ μs V/ μs
FPBW	Full Power Bandwidth	$6V_{P-P}$ (Note 6)		40		MHz
GBW	Gain Bandwidth Product	$f = 200\text{kHz}$, $R_L = 500\Omega$ $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	75 65 60	100		MHz MHz MHz
-3dB BW	-3dB Bandwidth	$A_V = 1$, $R_L = 500\Omega$		200		MHz
t_r , t_f	Rise Time, Fall Time	$A_V = 1$, 10% to 90%, 0.1V, $R_L = 100\Omega$		2		ns
t_{PD}	Propagation Delay (Note 10)	$A_V = 1$, 50% to 50%, 0.1V, $R_L = 100\Omega$		2.8		ns
OS	Overshoot	$A_V = 1$, 0.1V, $R_L = 100\Omega$		25		%
t_S	Settling Time	$A_V = -1$, 0.1%, 5V		30		ns
THD	Total Harmonic Distortion	$A_V = 2$, $f = 1\text{MHz}$, $V_{OUT} = 2V_{P-P}$, $R_L = 500\Omega$		-76		dB
dG	Differential Gain	$A_V = 2$, $V_{OUT} = 2V_{P-P}$, $R_L = 150\Omega$		0.12		%
dP	Differential Phase	$A_V = 2$, $V_{OUT} = 2V_{P-P}$, $R_L = 150\Omega$		0.07		DEG
R_{OUT}	Output Resistance	$A_V = 1$, $f = 1\text{MHz}$		0.4		Ω
	Channel Separation	$V_{OUT} = \pm 3\text{V}$, $R_L = 100\Omega$ $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	82 81 80	100		dB dB dB
I_S	Supply Current	Per Amplifier $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●		3	3.6 4.5 5.0	mA mA mA
		Per Amplifier, $V_S = \pm 6.5\text{V}$, (LT1813HV only) $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●			4.0 5.0 5.5	mA mA mA

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V_S = 5\text{V}$, $V_{CM} = 2.5\text{V}$, R_L to 2.5V , unless otherwise noted. (Note 8)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
V_{OS}	Input Offset Voltage (Note 4)	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	0.7	2.0	mV
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		2.5	mV
					3.5	mV
$\frac{\Delta V_{OS}}{\Delta T}$	Input Offset Voltage Drift (Note 7)	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	10	15	$\mu\text{V}/^\circ\text{C}$
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	10	30	$\mu\text{V}/^\circ\text{C}$
I_{OS}	Input Offset Current	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	50	400	nA
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		500	nA
					600	nA
I_B	Input Bias Current	$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	-1	± 4	μA
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		± 5	μA
					± 6	μA
e_n	Input Noise Voltage Density	$f = 10\text{kHz}$		8		$\text{nV}/\sqrt{\text{Hz}}$
i_n	Input Noise Current Density	$f = 10\text{kHz}$		1		$\text{pA}/\sqrt{\text{Hz}}$
R_{IN}	Input Resistance	$V_{CM} = 3.5\text{V}$ Differential		3	10	$\text{M}\Omega$
					1.5	$\text{M}\Omega$
C_{IN}	Input Capacitance			2		pF
V_{CM}	Input Voltage Range (Positive)	Guaranteed by CMRR $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	3.5	4.2	V
	Input Voltage Range (Negative)	Guaranteed by CMRR $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	0.8	1.5	V
CMRR	Common Mode Rejection Ratio	$V_{CM} = 1.5\text{V to } 3.5\text{V}$		73	82	dB
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	71		dB
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	70		dB
	Minimum Supply Voltage	Guaranteed by PSRR $T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	2.5	4	V
					4	V
A_{VOL}	Large-Signal Voltage Gain	$V_{OUT} = 1.5\text{V to } 3.5\text{V}$, $R_L = 500\Omega$		1.0	2	V/mV
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	0.7		V/mV
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	0.6		V/mV
		$V_{OUT} = 1.5\text{V to } 3.5\text{V}$, $R_L = 100\Omega$		0.7	1.5	V/mV
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	0.5		V/mV
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	0.4		V/mV
V_{OUT}	Maximum Output Swing (Positive)	$R_L = 500\Omega$, 30mV Overdrive		3.9	4.1	V
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	3.8		V
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	3.7		V
	Maximum Output Swing (Positive)	$R_L = 100\Omega$, 30mV Overdrive		3.7	3.9	V
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●	3.6		V
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●	3.5		V
	Maximum Output Swing (Negative)	$R_L = 500\Omega$, 30mV Overdrive		0.9	1.1	V
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●		1.2	V
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		1.3	V
		$R_L = 100\Omega$, 30mV Overdrive		1.1	1.3	V
		$T_A = 0^\circ\text{C to } 70^\circ\text{C}$	●		1.4	V
		$T_A = -40^\circ\text{C to } 85^\circ\text{C}$	●		1.5	V

ELECTRICAL CHARACTERISTICS

The ● denotes the specifications which apply over the full operating temperature range, otherwise specifications are at $T_A = 25^\circ\text{C}$. $V_S = 5\text{V}$, $V_{CM} = 2.5\text{V}$, R_L to 2.5V, unless otherwise noted. (Note 8)

SYMBOL	PARAMETER	CONDITIONS	MIN	TYP	MAX	UNITS
I_{OUT}	Maximum Output Current	$V_{OUT} = 1.5\text{V}$ or 3.5V , 30mV Overdrive $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	± 25 ± 20 ± 17	± 35		mA mA mA
I_{SC}	Output Short-Circuit Current	$V_{OUT} = 2.5\text{V}$, 1V Overdrive (Note 3) $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	± 55 ± 45 ± 40	± 75		mA mA mA
SR	Slew Rate	$A_V = -1$ (Note 5) $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	200 150 125	350		V/ μs V/ μs V/ μs
FPBW	Full Power Bandwidth	$2V_{P-P}$ (Note 6)		55		MHz
GBW	Gain Bandwidth Product	$f = 200\text{kHz}$, $R_L = 500\Omega$ $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	65 55 50	94		MHz MHz MHz
-3dB BW	-3dB Bandwidth	$A_V = 1$, $R_L = 500\Omega$		180		MHz
t_r , t_f	Rise Time, Fall Time	$A_V = 1$, 10% to 90%, 0.1V, $R_L = 100\Omega$		2.1		ns
t_{PD}	Propagation Delay (Note 10)	$A_V = 1$, 50% to 50%, 0.1V, $R_L = 100\Omega$		3		ns
OS	Overshoot	$A_V = 1$, 0.1V, $R_L = 100\Omega$		25		%
t_s	Settling Time	$A_V = -1$, 0.1%, 2V		30		ns
THD	Total Harmonic Distortion	$A_V = 2$, $f = 1\text{MHz}$, $V_{OUT} = 2V_{P-P}$, $R_L = 500\Omega$		-75		dB
dG	Differential Gain	$A_V = 2$, $V_{OUT} = 2V_{P-P}$, $R_L = 150\Omega$		0.22		%
dP	Differential Phase	$A_V = 2$, $V_{OUT} = 2V_{P-P}$, $R_L = 150\Omega$		0.21		DEG
R_{OUT}	Output Resistance	$A_V = 1$, $f = 1\text{MHz}$		0.45		Ω
	Channel Separation	$V_{OUT} = 1.5\text{V}$ to 3.5V , $R_L = 100\Omega$ $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●	81 80 79	100		dB dB dB
I_S	Supply Current	Per Amplifier $T_A = 0^\circ\text{C}$ to 70°C ● $T_A = -40^\circ\text{C}$ to 85°C ●		2.9	4.0 5.0 5.5	mA mA mA

Note 1: Absolute Maximum Ratings are those values beyond which the life of the device may be impaired.

Note 2: Differential inputs of $\pm 6\text{V}$ are appropriate for transient operation only, such as during slewing. Large sustained differential inputs can cause excessive power dissipation and may damage the part.

Note 3: A heat sink may be required to keep the junction temperature below absolute maximum when the output is shorted indefinitely.

Note 4: Input offset voltage is pulse tested and is exclusive of warm-up drift.

Note 5: Slew rate is measured between $\pm 2\text{V}$ at the output with $\pm 3\text{V}$ input for $\pm 5\text{V}$ supplies and $2V_{P-P}$ at the output with a $3V_{P-P}$ input for single 5V supplies.

Note 6: Full power bandwidth is calculated from the slew rate:

$$FPBW = SR/2\pi V_P$$

Note 7: This parameter is not 100% tested

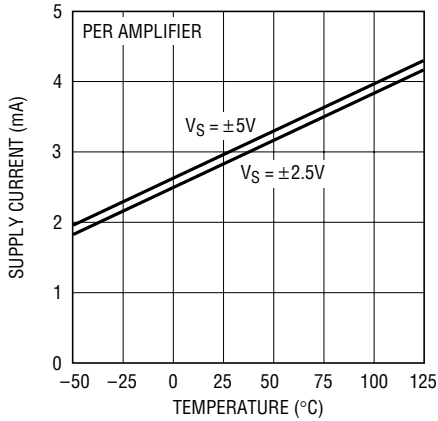
Note 8: The LT1813C/LT1814C are guaranteed to meet specified performance from 0°C to 70°C and is designed, characterized and expected to meet the extended temperature limits, but is not tested at -40°C and 85°C . The LT1813I/LT1814I are guaranteed to meet the extended temperature limits.

Note 9: The LT1813D is 100% production tested at 25°C . It is designed, characterized and expected to meet the 0°C to 70°C specifications although it is not tested or QA sampled at these temperatures. The LT1813D is guaranteed functional from -40°C to 85°C but may not meet those specifications.

Note 10: Propagation delay is measured from the 50% point on the input waveform to the 50% point on the output waveform.

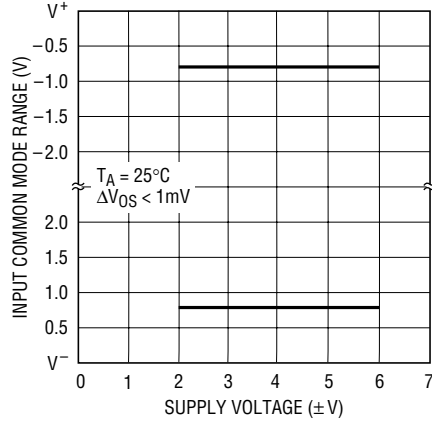
TYPICAL PERFORMANCE CHARACTERISTICS

Supply Current vs Temperature



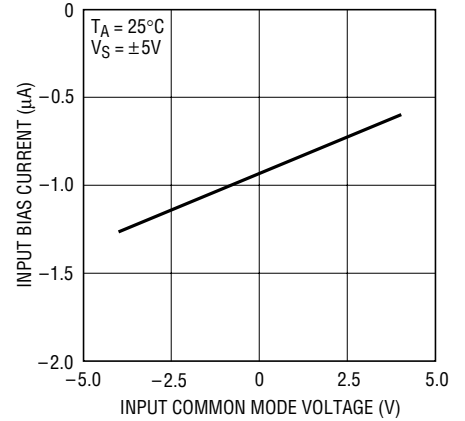
1813/14 G01

Input Common Mode Range vs Supply Voltage



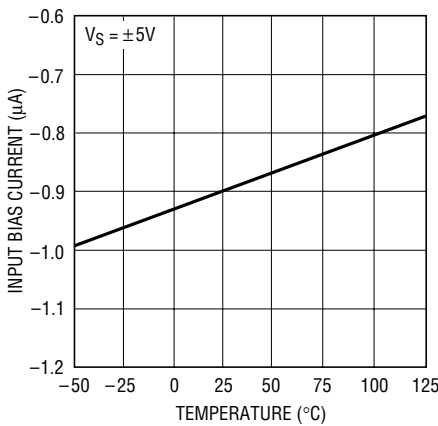
1813/14 G02

Input Bias Current vs Common Mode Voltage



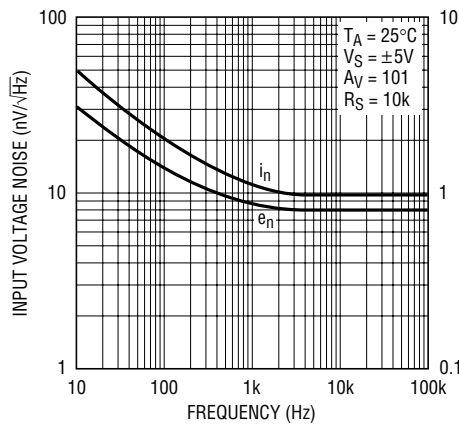
1813/14 G03

Input Bias Current vs Temperature



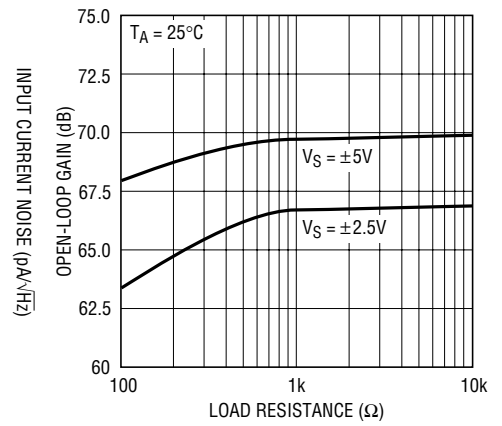
1813/14 G04

Input Noise Spectral Density



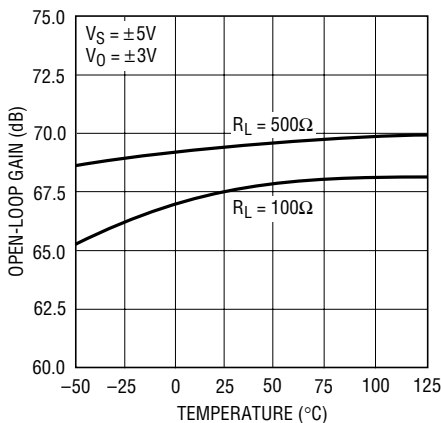
1813/14 G05

Open-Loop Gain vs Resistive Load



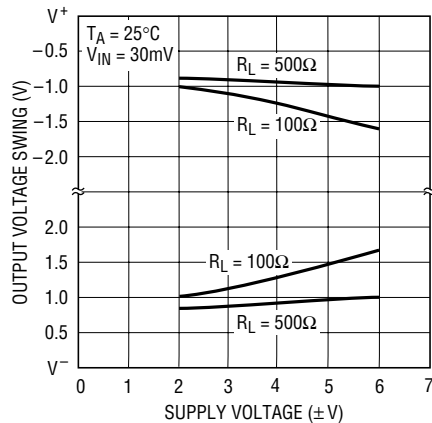
1813/14 G06

Open-Loop Gain vs Temperature



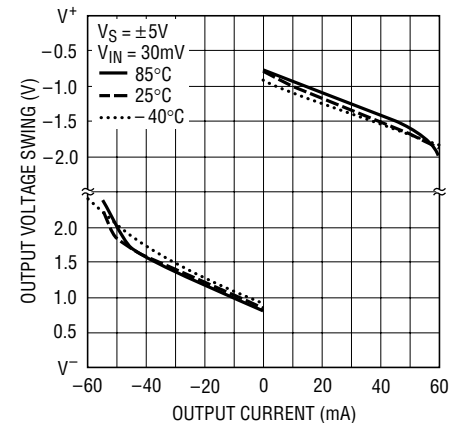
1813/14 G07

Output Voltage Swing vs Supply Voltage



1813/14 G02

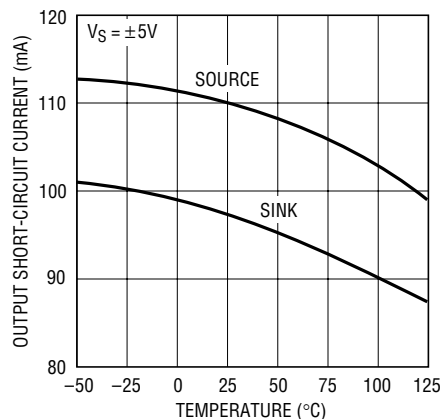
Output Voltage Swing vs Load Current



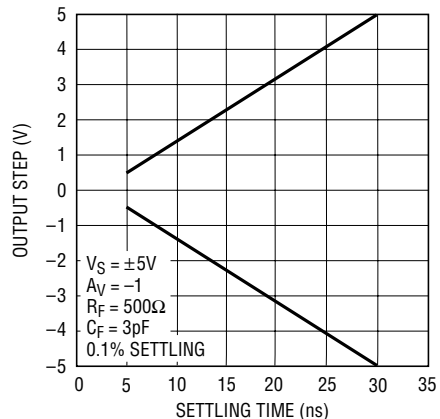
1813/14 G09

TYPICAL PERFORMANCE CHARACTERISTICS

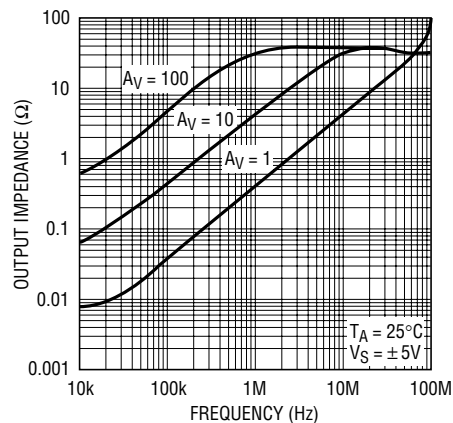
Output Short-Circuit Current vs Temperature



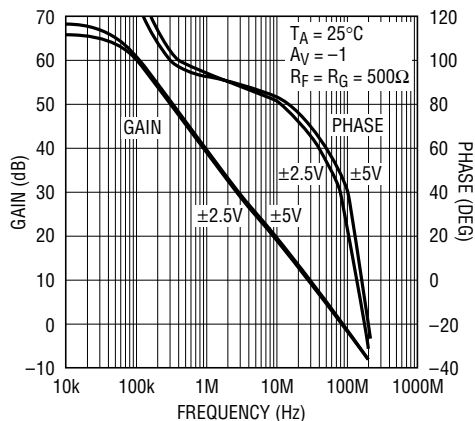
Settling Time vs Output Step



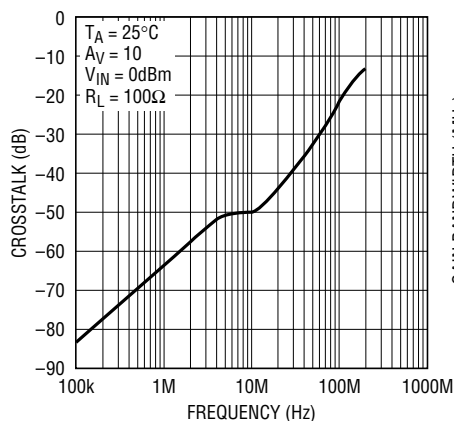
Output Impedance vs Frequency



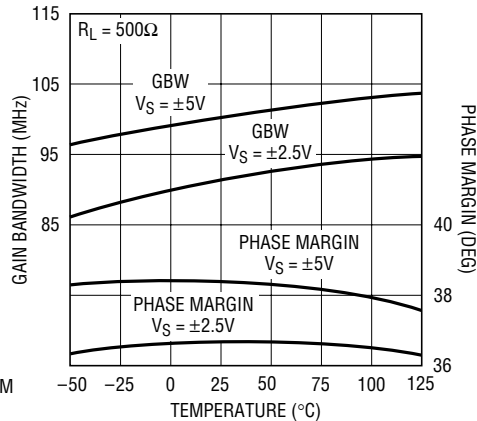
Gain and Phase vs Frequency



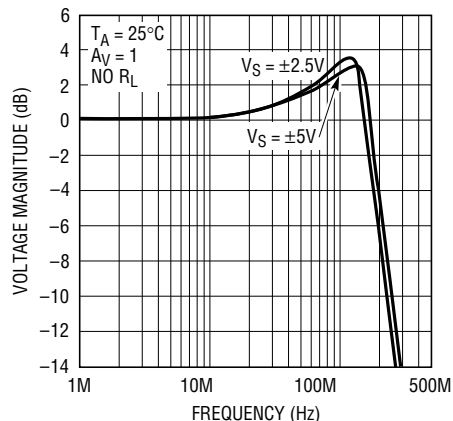
Crosstalk vs Frequency



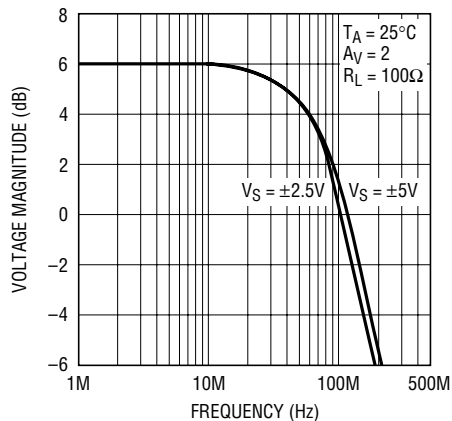
Gain Bandwidth and Phase Margin vs Temperature



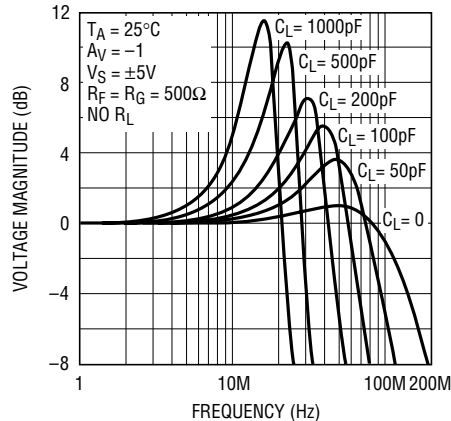
Frequency Response vs Supply Voltage, $A_V = 1$



Frequency Response vs Supply Voltage, $A_V = 2$

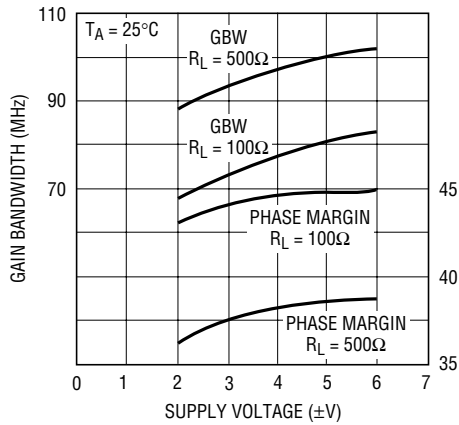


Frequency Response vs Capacitive Load, $A_V = -1$

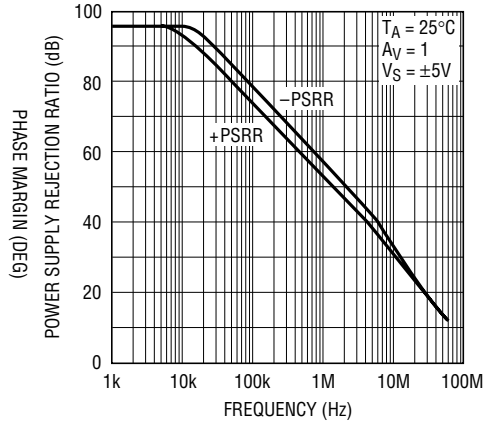


TYPICAL PERFORMANCE CHARACTERISTICS

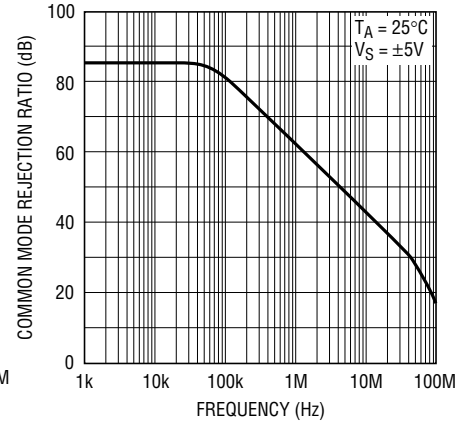
Gain Bandwidth and Phase Margin vs Supply Voltage



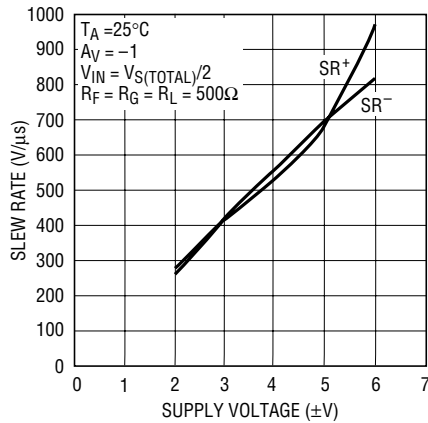
Power Supply Rejection Ratio vs Frequency



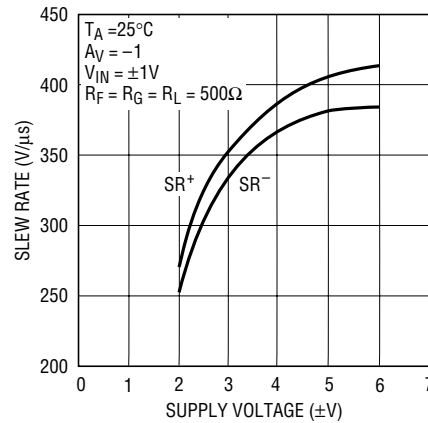
Common Mode Rejection Ratio vs Frequency



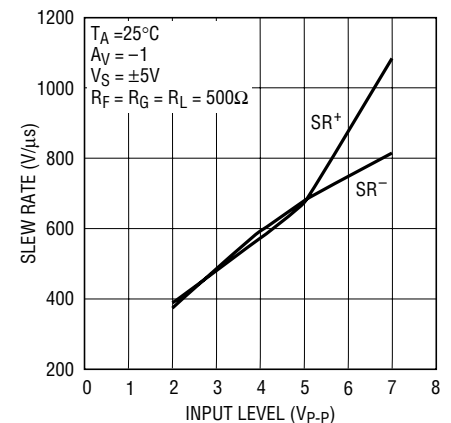
Slew Rate vs Supply Voltage



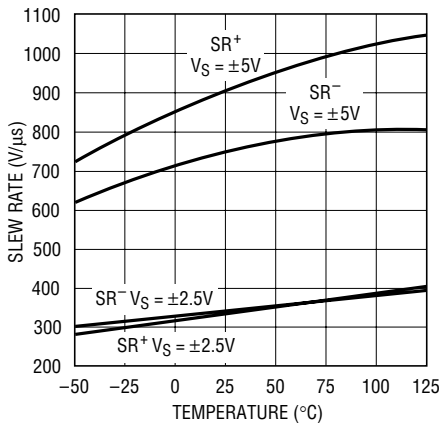
Slew Rate vs Supply Voltage



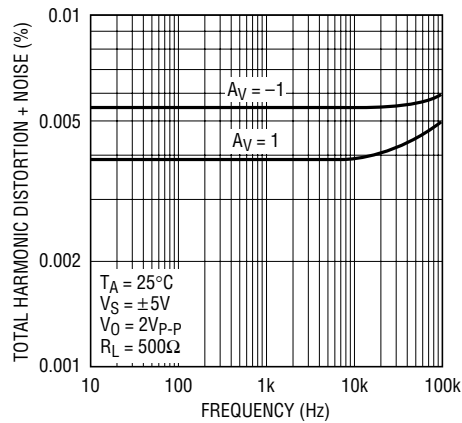
Slew Rate vs Input Level



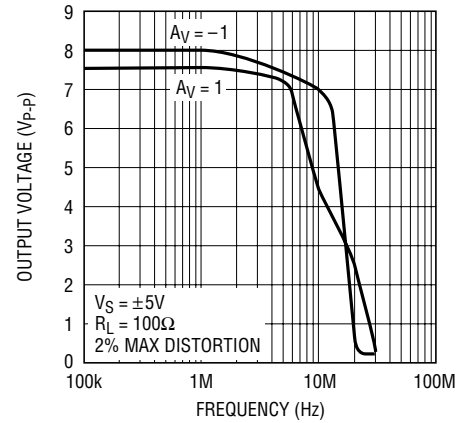
Slew Rate vs Temperature



Total Harmonic Distortion + Noise vs Frequency

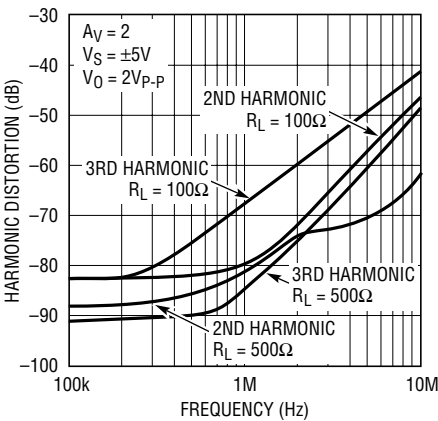


Undistorted Output Swing vs Frequency



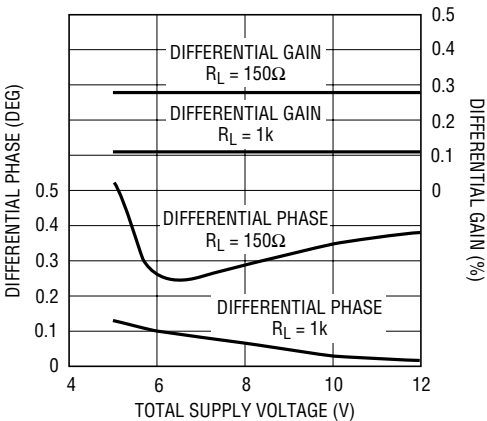
TYPICAL PERFORMANCE CHARACTERISTICS

2nd and 3rd Harmonic Distortion vs Frequency



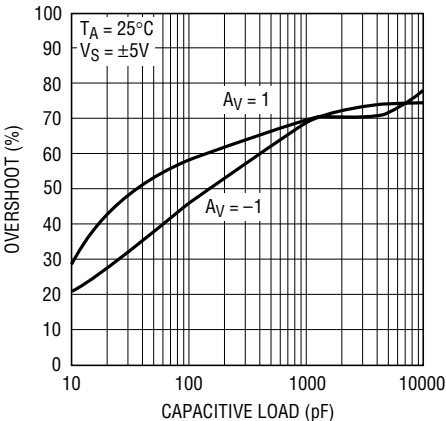
1813/14 G28

Differential Gain and Phase vs Supply Voltage



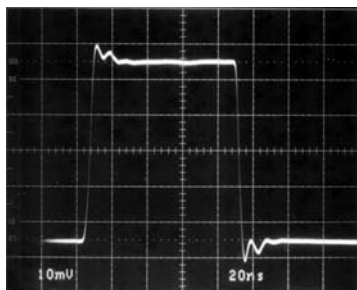
1813/14 G29

Capacitive Load Handling



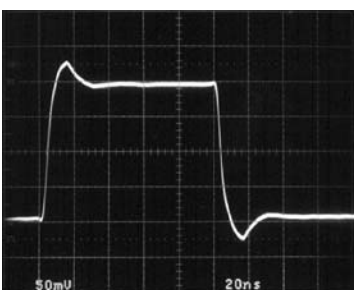
1813/14 G30

Small-Signal Transient ($A_V = 1$)



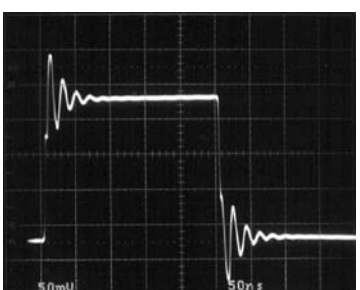
1813/14 G31

Small-Signal Transient ($A_V = -1$)



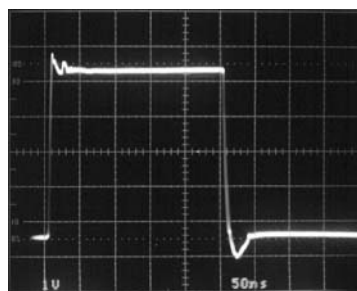
1813/14 G32

Small-Signal Transient ($A_V = 1$, $C_L = 100pF$)



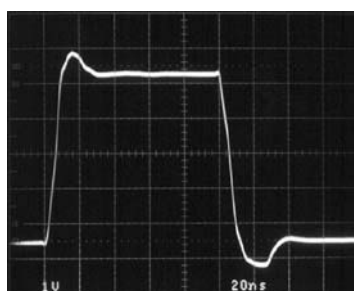
1813/14 G33

Large-Signal Transient ($A_V = 1$)



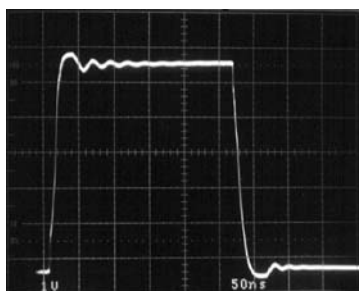
1813/14 G34

Large-Signal Transient ($A_V = -1$)



1813/14 G35

Large-Signal Transient ($A_V = -1$, $C_L = 200pF$)



1813/14 G36

APPLICATIONS INFORMATION

Layout and Passive Components

The LT1813/LT1814 amplifiers are more tolerant of less than ideal board layouts than other high speed amplifiers. For optimum performance, a ground plane is recommended and trace lengths should be minimized, especially on the negative input lead.

Low ESL/ESR bypass capacitors should be placed directly at the positive and negative supply pins (0.01μF ceramics are recommended). For high drive current applications, additional 1μF to 10μF tantalums should be added.

The parallel combination of the feedback resistor and gain setting resistor on the inverting input combine with the input capacitance to form a pole that can cause peaking or even oscillations. If feedback resistors greater than 1k are used, a parallel capacitor of value:

$$C_F > R_G \cdot C_{IN}/R_F$$

should be used to cancel the input pole and optimize dynamic performance. For applications where the DC noise gain is 1 and a large feedback resistor is used, C_F should be greater than or equal to C_{IN} . An example would be an I-to-V converter.

Input Considerations

The inputs of the LT1813/LT1814 amplifiers are connected to the base of an NPN and PNP bipolar transistor in parallel. The base currents are of opposite polarity and provide first order bias current cancellation. Due to variation in the matching of NPN and PNP beta, the polarity of the input bias current can be positive or negative. The offset current, however, does not depend on beta matching and is tightly controlled. Therefore, the use of balanced source resistance at each input is recommended for applications where DC accuracy must be maximized. For example, with a 100Ω source resistance at each input, the 400nA maximum offset current results in only 40μV of extra offset, while without balance the 4μA maximum input bias current could result in a 0.4mV offset contribution.

The inputs can withstand differential input voltages of up to 6V without damage and without needing clamping or

series resistance for protection. This differential input voltage generates a large internal current (up to 40mA), which results in the high slew rate. In normal transient closed-loop operation, this does not increase power dissipation significantly because of the low duty cycle of the transient inputs. Sustained differential inputs, however, will result in excessive power dissipation and therefore **this device should not be used as a comparator.**

Capacitive Loading

The LT1813/LT1814 are stable with capacitive loads from 0pF to 1000pF, which is outstanding for a 100MHz amplifier. The internal compensation circuitry accomplishes this by sensing the load induced output pole and adding compensation at the amplifier gain node as needed. As the capacitive load increases, both the bandwidth and phase margin decrease so there will be peaking in the frequency domain and ringing in the transient response. Coaxial cable can be driven directly, but for best pulse fidelity a resistor of value equal to the characteristic impedance of the cable (e.g., 75Ω) should be placed in series with the output. The receiving end of the cable should be terminated with the same value resistance to ground.

Slew Rate

The slew rate of the LT1813/LT1814 is proportional to the differential input voltage. Highest slew rates are therefore seen in the lowest gain configurations. For example, a 5V output step in a gain of 10 has a 0.5V input step, whereas in unity gain there is a 5V input step. The LT1813/LT1814 is tested for a slew rate in a gain of –1. Lower slew rates occur in higher gain configurations.

Power Dissipation

The LT1813/LT1814 combine two or four amplifiers with high speed and large output drive in a small package. It is possible to exceed the maximum junction temperature specification under certain conditions. Maximum junction temperature (T_J) is calculated from the ambient temperature (T_A) and power dissipation (P_D) as follows:

$$T_J = T_A + (P_D \cdot \theta_{JA})$$

APPLICATIONS INFORMATION

Power dissipation is composed of two parts. The first is due to the quiescent supply current and the second is due to on-chip dissipation caused by the load current. The worst-case load induced power occurs when the output voltage is at 1/2 of either supply voltage (or the maximum swing if less than 1/2 the supply voltage). Therefore P_{DMAX} is:

$$P_{DMAX} = (V^+ - V^-) \cdot (I_{SMAX}) + (V^+/2)^2/R_L \text{ or}$$

$$P_{DMAX} = (V^+ - V^-) \cdot (I_{SMAX}) + (V^+ - V_{OMAX}) \cdot (V_{OMAX}/R_L)$$

Example: LT1814S at 70°C, $V_S = \pm 5V$, $R_L = 100\Omega$

$$P_{DMAX} = (10V) \cdot (4.5mA) + (2.5V)^2/100\Omega = 108mW$$

$$T_{JMAX} = 70^\circ C + (4 \cdot 108mW) \cdot (100^\circ C/W) = 113^\circ C$$

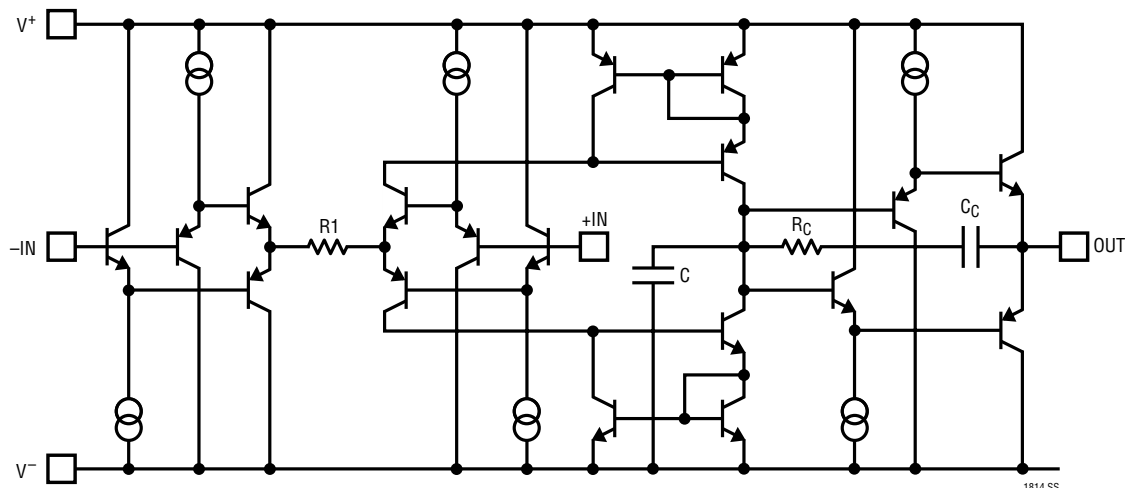
Circuit Operation

The LT1813/LT1814 circuit topology is a true voltage feedback amplifier that has the slewing behavior of a current feedback amplifier. The operation of the circuit can be understood by referring to the Simplified Schematic. Complementary NPN and PNP emitter followers buffer the inputs and drive an internal resistor. The input voltage appears across the resistor, generating current that is mirrored into the high impedance node.

Complementary followers form an output stage that buffers the gain node from the load. The input resistor, input stage transconductance, and the capacitor on the high impedance node determine the bandwidth. The slew rate is determined by the current available to charge the gain node capacitance. This current is the differential input voltage divided by R_1 , so the slew rate is proportional to the input step. Highest slew rates are therefore seen in the lowest gain configurations.

The RC network across the output stage is bootstrapped when the amplifier is driving a light or moderate load and has no effect under normal operation. When a heavy load (capacitive or resistive) is driven, the network is incompletely bootstrapped and adds to the compensation at the high impedance node. The added capacitance moves the unity-gain frequency away from the pole formed by the output impedance and the capacitive load. The zero created by the RC combination adds phase to ensure that the total phase lag does not exceed 180° (zero phase margin), and the amplifier remains stable. In this way, the LT1813/LT1814 are stable with up to 1000pF capacitive loads in unity gain, and even higher capacitive loads in higher closed-loop gain configurations.

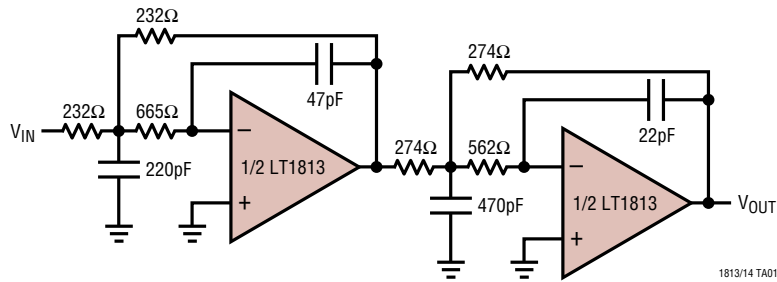
SIMPLIFIED SCHEMATIC (one amplifier)



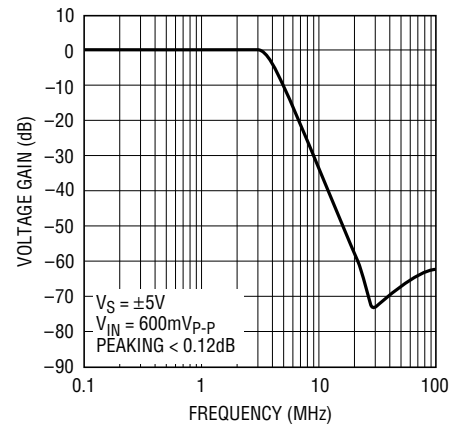
1814 SS

TYPICAL APPLICATION

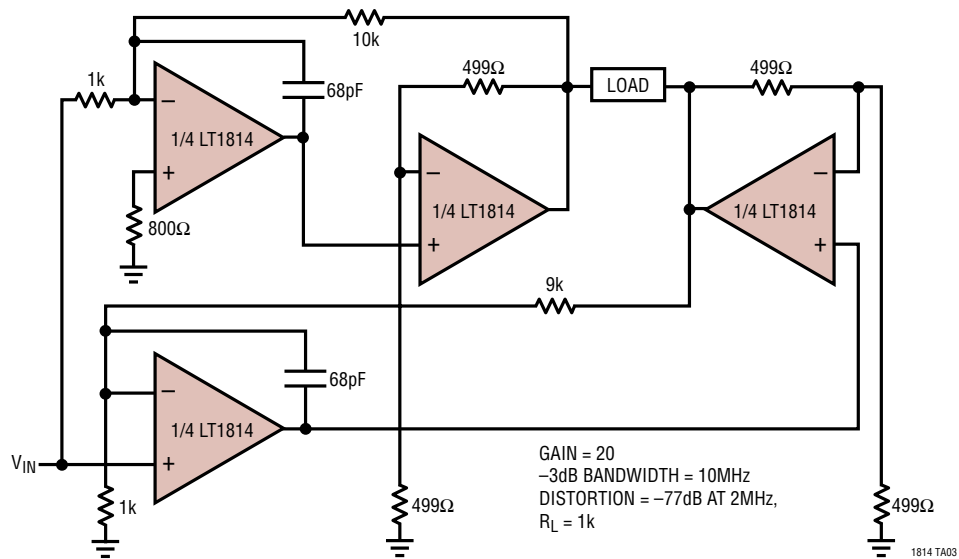
4MHz, 4th Order Butterworth Filter



Filter Frequency Response

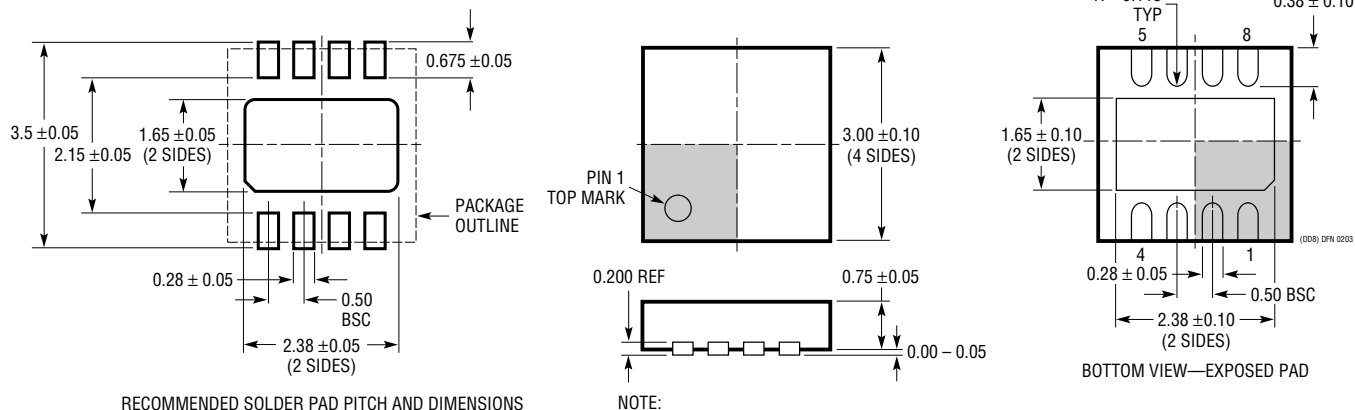


Gain of 20 Composite Amplifier Drives Differential Load with Low Distortion



PACKAGE DESCRIPTION

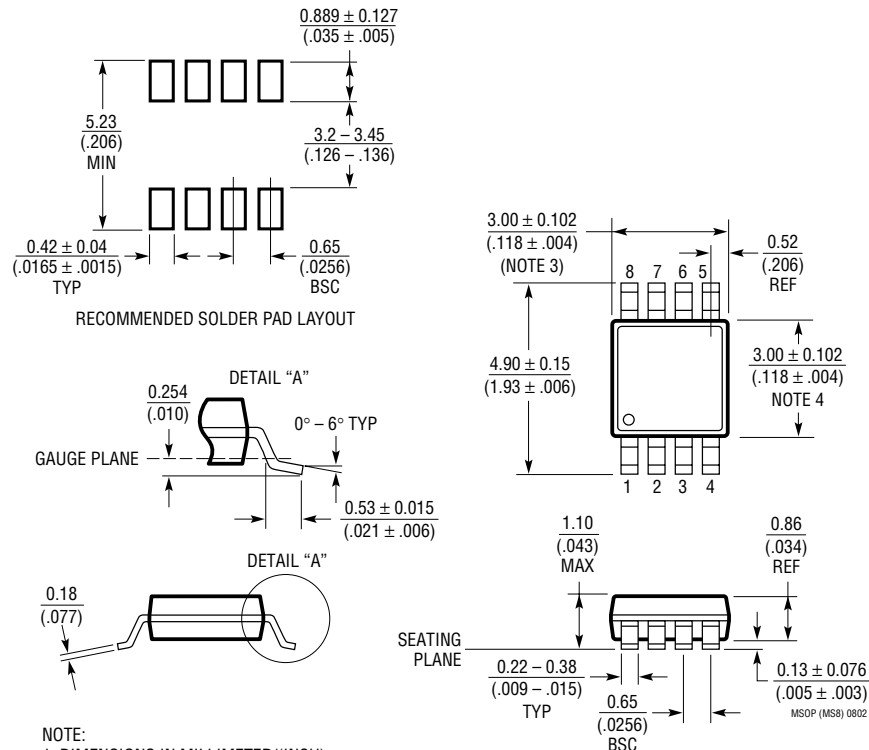
DD Package 8-Lead Plastic DFN (3mm × 3mm) (Reference LTC DWG # 05-08-1698)



NOTE:

1. DRAWING TO BE MADE A JEDEC PACKAGE OUTLINE MO-229 VARIATION OF (WEED-1)
2. ALL DIMENSIONS ARE IN MILLIMETERS
3. DIMENSIONS OF EXPOSED PAD ON BOTTOM OF PACKAGE DO NOT INCLUDE MOLD FLASH. MOLD FLASH, IF PRESENT, SHALL NOT EXCEED 0.15mm ON ANY SIDE
4. EXPOSED PAD SHALL BE SOLDER PLATED

MS8 Package 8-Lead Plastic MSOP (Reference LTC DWG # 05-08-1660)

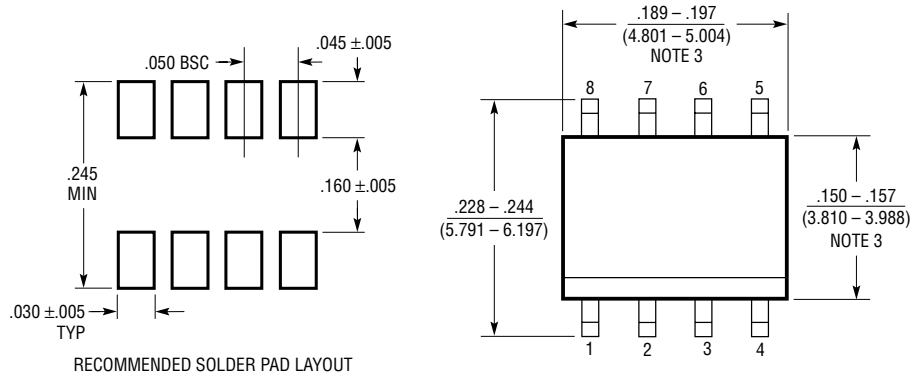


NOTE:

1. DIMENSIONS IN MILLIMETER/(INCH)
2. DRAWING NOT TO SCALE
3. DIMENSION DOES NOT INCLUDE MOLD FLASH, PROTRUSIONS OR GATE BURRS. MOLD FLASH, PROTRUSIONS OR GATE BURRS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
4. DIMENSION DOES NOT INCLUDE INTERLEAD FLASH OR PROTRUSIONS. INTERLEAD FLASH OR PROTRUSIONS SHALL NOT EXCEED 0.152mm (.006") PER SIDE
5. LEAD COPLANARITY (BOTTOM OF LEADS AFTER FORMING) SHALL BE 0.102mm (.004") MAX

PACKAGE DESCRIPTION

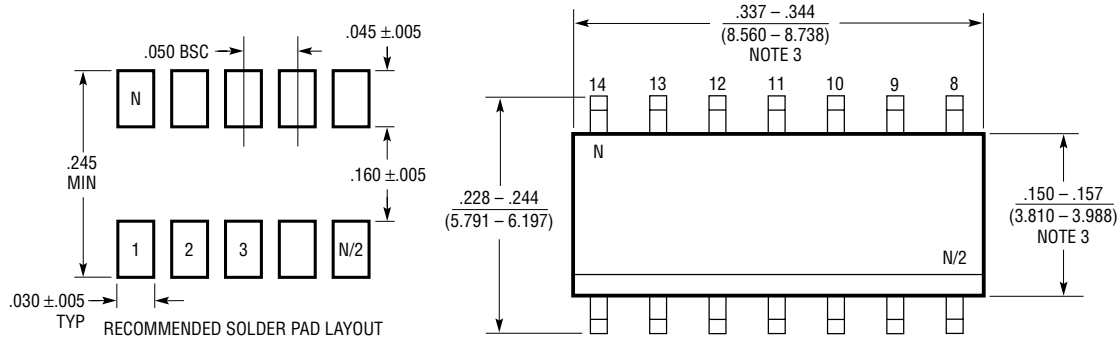
S8 Package 8-Lead Plastic Small Outline (Narrow .150 Inch) (Reference LTC DWG # 05-08-1610)



- NOTE:
1. DIMENSIONS IN INCHES
(MILLIMETERS)
2. DRAWING NOT TO SCALE
3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

S08 0303

S Package 14-Lead Plastic Small Outline (Narrow .150 Inch) (Reference LTC DWG # 05-08-1610)



- NOTE:
1. DIMENSIONS IN INCHES
(MILLIMETERS)
2. DRAWING NOT TO SCALE
3. THESE DIMENSIONS DO NOT INCLUDE MOLD FLASH OR PROTRUSIONS.
MOLD FLASH OR PROTRUSIONS SHALL NOT EXCEED .006" (0.15mm)

S14 0502

TYPICAL APPLICATION

The circuit diagram shows two LT1813 op-amp halves. The first half (labeled 1/2 LT1813) is configured as an inverting amplifier with a gain of -10. Its non-inverting input (+) is grounded, and its inverting input (-) is connected to the input signal V_{IN} through a resistor $R1$ (10k) and to its output through a feedback resistor $R2$ (1k). The output of the first stage is connected to the inverting input of the second half (also labeled 1/2 LT1813) through a resistor $R3$ (1k). The second stage is also configured as an inverting amplifier with a gain of -1, with its non-inverting input (+) grounded and its output connected to the output signal V_{OUT} through a feedback resistor $R4$ (10k). A resistor $R5$ (220Ω) is connected between the output of the first stage and the inverting input of the second stage, in parallel with $R3$.

$$\text{GAIN} = \left[\frac{R_4}{R_3} \right] \left[1 + \left(\frac{1}{2} \right) \left(\frac{R_2}{R_1} + \frac{R_3}{R_4} \right) + \frac{(R_2 + R_3)}{R_5} \right] = 102$$

1813/14 TA03

GN16 (SSOP) 0502

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